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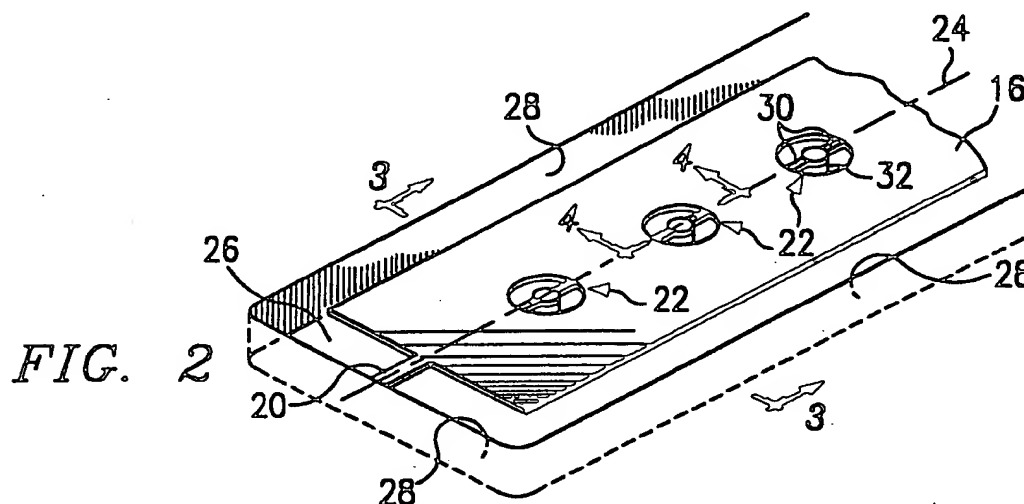
Remarks:

This application was filed on 27 - 06 - 1996 as a
divisional application to the application mentioned
under INID code 62.

(54) Apparatus for directing light

(57) The method disclosed comprises the steps of
directing light to a spatial light modulator comprising a
plurality of modulators where each modulator com-
prises a plurality of individual mirrors (16) rotatably fixed
to at least two support members (20,22) displaced from
an edge of the mirror. This deformable mirror device fur-

ther comprises an electrode for rotating the mirror,
selecting an angle through which the mirror is to rotate,
generating a signal characteristic of the angle, applying
the characteristic signal to the electrode, and rotating
the mirror through the selected angle.



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Description

TECHNICAL FIELD OF THE INVENTION

This invention relates in general to electro-optical devices, and more particularly, to a device for directing light and to a method of manufacturing a spatial light modulator.

BACKGROUND OF THE INVENTION

Visible light may be accurately positioned or "steered" by at least three classes of electro-optical devices; galvanometric scanners, resonant mirrors, and rotating polygon mirrors.

Galvanometric scanners reflect light off of a mirror which may be rotated about an axis through a small angle by application of an electrical current situated in the presence of a fixed magnetic field. The electrical current generates a magnetic field proportional to the current and the interaction of the two magnetic fields causes the electrical lead conducting the electrical current to twist relative to the fixed magnetic field. This twisting motion can be advantageously linked to a small mirror by which incident light may be steered.

Resonant mirrors similarly reflect light off of a mirror which is caused to move by the application of an electrical signal. Here, however, the electrical signal drives a subcomponent such as a voice coil from an audio speaker. The voice coil in turn pushes against a spring-mounted hinged mirror. The mirror typically has attached to it a counterweight such that the resonant frequency of the counterweight and mirror assembly acts like a tuning fork. The mirror can then be made to oscillate at a resonant frequency to steer incident light in a periodic fashion. These two classes of devices are typically used in applications such as flying spot scanners and laser printers.

The rotating polygon mirror is a multi-faceted mirror rotated at high speed by a precision motor. As each facet subtends a light beam from a laser source, it scans it through an arc with a typical included angle up to about 120 degrees. The mirror elements are generally facets cut onto the peripheries of a wheel, though often shapes are sometimes encountered. The laser polygon is most often used in laser xerographic printer systems as the optical scanner, converting digital inputs into patterns of light on a photoreceptor surface. The patterns are subsequently developed and printed onto paper.

Galvanometric scanners, resonant mirrors, and polygon mirrors have disadvantages when used to steer light. All three classes of devices are relatively large, are expensive, and are susceptible to shock and vibration. These limitations preclude their use in many consumer applications and where component size is a constraint. Galvanometric scanners and resonant scanners are generally slow responding and are also typically sus-

ceptible to changes in the scanner's motion. This precludes their use in most mobile environments.

Another electro-optical device known to those skilled in the art is a spatial light modulator such as a deformable mirror device ("DMD"). While DMD's have been used in some light steering applications they suffer from the disadvantage of being too small for many applications. A typical DMD mirror is on the order of $12 \times 12 \mu\text{m}^2$. A useful light steering device should be in the range of $1.27 \times 0.25 \text{ cm}^2$. In attempting to increase the size of DMD's a significant problem arises as a result of the mirror distortion. Typically, DMD's are supported at two edges. Due to the increased size of such a large DMD, they will distort under the influence of the applied operating voltage, making them useless.

Therefore, a need has arisen for an apparatus for steering light which is very compact, inexpensive, power efficient, and suitable for use in a non-stationary environment.

SUMMARY OF THE INVENTION

In accordance with the present invention, an apparatus is provided which substantially eliminates and reduces the disadvantages and problems associated with prior resonant mirrors, galvanometric scanners, laser polygon scanners and DMDs.

An apparatus is disclosed provided with the features of claim 1.

A first technical advantage of the disclosed invention is its size. In one embodiment of the invention, a full featured modulator for use in an apparatus for light steering is disclosed that is the size of a typical integrated circuit package.

A second technical advantage of the invention is its power consumption. The disclosed device is electrostatic in nature, and thus consumes negligible power. The invention therefore additionally benefits from lower heat generation and better safety characteristics.

A third advantage is speed of response. Because the mirror is fabricated using a thin-film semiconductor process, the total mass is much lower than mirrors fabricated on conventional substrates.

A final technical advantage of the disclosed invention is its portability. When properly packaged, the resonant mirror may be used in a mobile environment with little or no degradation of performance or threat of premature system failure.

BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the present invention and the advantages thereof, reference is now made to the following description taken in conjunction with the accompanying drawings in which:

FIGURE 1 depicts perspective a first embodiment of the disclosed invention;

FIGURE 2 illustrates perspectively the mirror element depicted in Figure 1;

FIGURES 3 and 4 illustrate, in cross-sectional view, the mirror element depicted in Figure 2 along lines 3-3 and 4-4 respectively;

FIGURES 5a through 5f illustrate, in cross-sectional view, sequential steps of the mirror element depicted in Figure 2 during fabrication;

FIGURE 6 depicts perspectively a second embodiment of the disclosed invention;

FIGURE 7 illustrates, in cross-sectional view, the second embodiment of the disclosed invention depicted in FIGURE 6 along line 7-7;

FIGURE 8 depicts perspectively a third embodiment of the disclosed invention; and

FIGURE 9 illustrates, in cross-sectional view, the third embodiment of the disclosed invention depicted in FIGURE 8 along line 9-9.

DETAILED DESCRIPTION OF THE INVENTION

The preferred embodiment of the present invention is illustrated in Figures 1 through 9 of the drawings, like numerals being used to refer to like and corresponding parts of the various drawings.

FIGURE 1 depicts perspectively beam steering device 10 containing one embodiment of the disclosed invention. Device 10 comprises a body 12, typically plastic, encasing a substrate 14 and a long thin deflectable mirror element 16. Substrate 14 typically contains a shallow well (shown in FIGURE 2) having a base and sidewalls from which mirror 16 is supported by flexible hinges (shown in FIGURE 2). The well allows mirror element 16 to rotate out of the plane containing the substrate and about the axis formed by the hinges all the while maintaining the flatness of mirror element 16. Schematically, a condenser system directs a beam of light 13 from light source 15 and a reflector 17 onto DMD 16 through lense 11.

In a practical application, light bundle 13 may be from any source of light, such as a laser, and may also contain image information. For example, lense 11 may be relaying light from another spatial light modulator (SLM) on to the DMD scanning mirror. The scanned light may subsequently converge to a focus at an image plane beyond device 10, with or without passing through an intermediate lense element.

Because the mirror element 16 operates substantially in the plane of substrate 14, it does not introduce a defocusing effect or any field curvature into the final image as is the case with the conventional scanners.

Device 10 also has connected to it a varying number of electrical leads 18 which connect it to other subcomponents. The number of leads 18 may vary depending on the level of sophistication of circuitry contained in device 10. For instance, substrate 14 might itself be a semiconductor and comprise an internal signal generator that controls the rate of rotation of mirror element 16. In such a case, device 10 might only need

three leads, ground, power, and on/off. Device 10 however, may also be designed to be driven by an external signal generator (shown in FIGURE 3). In such a case, additional pins may be needed to control the motion of mirror element 16 and the substrate need not be a semiconductor.

In operation, a beam of collimated light 13 is directed to the top face of device 10 where it reflects off of mirror element 16. Mirror element 16 is then made to twist or rotate about an axis defined by its supports such that the reflected light is steered through twice the angle of rotation. Mirror element 16 will have associated with it a natural frequency of rotation, its "resonant frequency", at which it will rotate with a minimum driving force. By advantageously controlling the physical dimensions and the materials of mirror element 16, the resonant frequency of mirror element 16 may be tailored for particular applications. The resonant frequency of mirror element 16 is given by the expression:

$$f = \frac{1}{2\pi} \sqrt{\frac{\tau/I}{\theta}}$$

or

$$f = \frac{1}{2\pi} \sqrt{K/I}$$

where I is the moment of inertia of the mirror element, τ is the peak vibrational torque reaction of the mirror at a peak amplitude θ , and K is the spring constant, τ/θ , a measure of the rotational stiffness of the hinge elements 16. The mechanical properties of simple geometries and most semiconductor materials are well known, and hence K and I can be determined for most situations.

The electro-mechanical properties of mirror element 16 may be incorporated into a wide variety of systems. For instance, device 10 may be used to repetitively steer a modulated laser beam onto a drum of a xerographic printer or universal product code ("UPC") scanner. In the first application, a laser beam is scanned onto a drum which is made to attract toner where it has been struck by the laser beam. The drum can then transfer the developed toner pattern onto plain paper to produce a printed image. In the latter application, a laser beam is scanned onto a product to be purchased by a consumer. The beam is reflected off of a series of spaced lines on the product and back to a photodiode detector. The scanner can then determine the identity of the product to be purchased by the pattern of lines and the consumer may be accordingly charged. The laser beam must be diverted to repetitively scan a volume of space so that the product identity may be determined regardless of the orientation to the laser beam.

In other applications, device 10 may be used as part of a virtual display system. In such a system, a series of rows of display pixels are sequentially projected onto the resonant mirror while the mirror is made

to oscillate. The series of rows may be produced by, for instance, a conventional deformable mirror device reflecting a white light source. By advantageously timing the output of the deformable mirror device and the position of the resonating mirror, an entire full page display may be made. The persistence of the viewer's eye will cause the viewer to perceive the series of adjacent lines as a full page display. Such a system is described in EP-A-0 547 493.

Finally, by scanning either a spot, or an array of suitably modulated light pulses, the exposure of a light sensitive media, such as photographic film, photoresist or any other photopolymer can be accomplished.

FIGURE 2 depicts perspective the left half of the mirror element 16 of Figure 1. It should be understood that although only the left portion of mirror element 16 is depicted, a symmetrical right portion is intended. Mirror element 16 is supported along its length by a series of axially aligned supports. For stability reasons, at least two supports must be used. These may be either located at the end of mirror 16 as is hinge element 20 or may be displaced from an edge of mirror element 16 as are supporting members 22. All of the supports are aligned along the line 24 forming the "axis" of rotation. These intermediate supporting members 22 stiffen mirror element 16 in the long dimension without impeding the rotation of mirror element 16 about its axis of rotation. As a result, mirror element 16 is generally planar with the top of well 26 or to the underlying substrate. Each supporting member is anchored to the base of the well and insures the flatness of mirror element 16 during operation. It should be understood that well 26 may, in fact, be etched from substrate 14 or may simply remain after fabrication of a layer or layers which form sidewalls 28. Sidewalls 28 are generally continuous around the perimeter of mirror element 16.

Without supporting member 22, mirror element 16 would sag into well 26 due to its relative great length and thin cross section. In operation, mirror element 16 would not rotate about its axis of rotation 24 when driven (as will be discussed below) but might simply sag downward further if it is fabricated without supporting member 22. Both of these results would interfere with the desired light steering capabilities of the device. Supporting member 22 itself comprises at least one hinge element 30 which connect mirror element 16 to a central post 32. In the preferred embodiment, supporting member 22 comprises two symmetrical hinge elements 30. These hinge members typically are made of the same material as hinge element 20 and mirror element 16.

FIGURE 3 depicts mirror element 16 taken along line 3-3 of FIGURE 2. Mirror element 16 is supported by a central post 32 in well 26. Central post 32 supports mirror element 16 from the base of well 32 along the axis of rotation 24. Device 10 also contains at least one electrode 34 displaced outwardly from the axis of rotation 24. A second complementary electrode 36 may be added to device 10 in a second position also displaced outwardly from the axis of rotation 24 and in a direction

generally opposite from the direction of electrode 34. As depicted, electrodes 34 and 36 are electrically connected to a signal generator 37. Because mirror element 16 and posts 32 can be electrically isolated from electrodes 34 and 36, an additional voltage can be applied to the mirror element 16 itself by signal generator 39 to accomplish other control functions well known to the DMD user, such as bias and reset. Signal generators 37 and 39 may be located within or without device 10.

Device 10 might also comprise one or two stops 38 displaced outwardly from electrodes 34 and 36 and held at the same electrical potential as mirror element 16. These stops are called landing electrodes and are positioned so that mirror element 16 will strike them before striking the electrodes 34 and 36 or any other part of device 10. This prevents an electrical current from flowing between mirror element 16 and the electrodes 34 and 36, or any other part, which would fuse the two together or cause other damage. It should be understood that the electrodes and stops may be single sets of small pads, multiple sets of small pads or long strips running generally parallel to the axis of rotation.

The periodic rotation of mirror element 16 about its axis of rotation 24 may be controlled by applying an alternating current between electrodes 34 and 36. The signals applied to electrodes 34 and 36, in the preferred embodiment, are 180° out of phase with each other and have a frequency equal to the resonant frequency of mirror element 16. Mirror element 16 is meanwhile held at an intermediate potential. The amplitude of rotation may be regulated by controlling the amplitude of the alternating waveform.

In the alternate, mirror 16 may be driven off resonance. In such a case, it is deflected in an analog fashion to about 50% of the maximum rotation angle. After that point, electrostatic attraction, which goes as the inverse square of the mirror 16 to electrode 34, 36 spacing, will overcome the linear restoring torque of hinges 30, and the mirror will land on landing electrode 38 at the full deflection angle. This is the digital mode of operation. The rate of rotation is controlled by mirror inertia, I, and damping due to the gas present in the cavity 26 with the mirror.

FIGURE 4 depicts a cross-sectional view of mirror element 16 of FIGURE 2 taken along the line 4-4. Here, mirror element 16 is connected to support post 32 by two thin hinge elements 30. Hinge elements 30 are partially covered by an oxide layer 40, a portion of which remains after manufacture as will be more fully described below. Central post 32 rests on electrically isolated pad 42 and layers 44 and 46. Substrate 46 may contain circuitry necessary to drive mirror element 16 about its axis of rotation as described above.

FIGURES 5a-5f illustrate, in cross-sectional view, sequential steps of the mirror element depicted in FIGURE 4 during fabrication.

(a) Initially, substrate layer 46 is prepared using conventional photolithographic techniques. Substrate layer may contain, for instance, an internal oscillator for driving mirror element 16 (FIGURES 1-4) or other control circuitry.

Each support post pad 42 is insulated from the underlying substrate by an insulator such as silicon dioxide layer 44, typically 200 nm thick. Post pad 42 is approximately 300 nm thick and is fabricated from an alloy of aluminum, titanium, and silicon ("Ti:Si:Al"). After the Ti:Si:Al is sputter deposited onto silicon oxide layer 44, it is patterned and plasma etched to define post pad 42, electrodes 34 and 36 and stops 38 (latter three shown in FIGURE 3).

(b) A photoresist is then spun on and baked in, typically, three applications to a total thickness of approximately 4 microns to form spacer 48. Three applications of, typically positive, resist are used to fill the thickness to avoid resist surface waves which can occur when spinning on a single, very thick layer. A bake of approximately 180°C is required after each application of resist to prevent the previous layers from dissolving in subsequent resist applications, to drive out excess solvent from the spacer and to avoid the formation of solvent bubbles under the hinge metal.

(c) Spacer 48 is etched to form a via that exposes each post pad 42.

(d) Approximately 80 nm of Ti:Si:Al is applied to spacer 48 to form part of each post and a thin hinge layer 50 from which the end hinges and central hinges are etched. The resistancy to twist, or flexibility of the hinges may be controlled by controlling their length, width and thickness as well as by controlling their composition. Typically, each hinge is two microns wide. The support post hinges are ten microns long. Next, 150 nm of silicon dioxide is deposited, patterned and etched to form hinge etch stops 52 over all future hinges.

(e) Approximately 360 nm of Ti:Si:Al is sputter deposited onto hinge layer 50 and hinge etch stops 52 to form mirror layer 54. The deposition of the metal of mirror layer 54 is made under the same conditions as for the deposition of hinge layer 50 so that no stresses between the metal layers are developed. The moment of inertia, I, of each mirror element 16 (shown in FIGURES 1-4) may be controlled by controlling their length, width and thickness as well as by controlling their composition. Typically, each mirror element is 0.64 cm wide and 2.54 cm long. Finally, an etch stop layer 56 is deposited on top of mirror layer 54 for protection during subsequent fabrication steps.

(f) A photoresist layer is applied to etch stop layer 56 and patterned to define plasma etch access holes 58 above hinge stops 52 (shown in FIGURE 5e). The patterned photoresist layer may then be used as a mask for plasma etching the mirror ele-

ment layer above each hinge stop. Access holes 58 appear as a set of "C's" facing one another when viewed from above. The plasma etch of the aluminum alloy may be made with a chlorine/boron trichloride/carbon trichloride etch gas mixture. After the remaining photoresist layer is removed, remaining etch stop layer 50 and the hinge etch stops 52 may be removed by an anisotropic etch.

Access holes 58 may be minimized by making them conform to the post and hinge dimensions, with a gap of only 1 or 2 microns separating the posts and hinges from mirror 16. This minimizes the optical effects of the post and hinge features on the mirror performance.

Spacer 48 is removed by, for instance, etching in oxygen with a few percent fluorine. The completed support post of the resonant mirror is depicted in FIGURE 4.

Optional end hinge 20 (depicted in FIGURE 2) is fabricated using the same steps as was the central post and hinge elements depicted in FIGURES 5a-5f. Each end hinge 20 is integrated into the surrounding of non-rotating mirror metal. In some applications, it may be preferable to eliminate the surrounding structure, so that only the active mirror element protrudes above the substrate layer 46. Support posts could be provided at mirror extreme ends in that case.

A practical limitation of the embodiment described relates to the limiting spacer thickness and support post heights achievable using reasonable semiconductor processes. The size of the via formed in FIGURE 5c is related by technical processes to the thickness of spacer layer 48. In general, the thicker the spacer layer the larger the subsequent via must be. The size of the via must be minimized, however, to minimize any optical aberrations in the resulting mirror element 16. This optical limitation, therefore, limits the thickness of spacer layer 48 and the maximum angle of rotation. Spacers of the prescribed 4 micron thickness will only permit rather small rotation angles for mirrors having any appreciable width. If a ± 10 degree rotation angle is desired, the width of the mirror can only be a factor of 12 times the thickness of the spacer layer 48 or about 50 microns.

FIGURES 6 and 7 depict an asymmetric mirror structure that overcomes the limitation on rotation. It can be operated only in one direction, but provides for a relatively wide mirror and reasonable angles of operation within the above spacer constraints.

FIGURES 8 and 9 depict a practical way to achieve large area mirrors, that can operate through angles of 10 degrees or greater, and meet the manufacturing constraints of spacer layer 48 and support posts 32. In this approach, mirrors of large extent are segmented into a reticulated array of long slender elements 16. Each mirror element 16 is supported on a line of supporting elements 22 as shown in FIGURE 3. Each mirror has the electrode 34 and stop 38 structure depicted in FIGURE 3 necessary to address the mirror.

The optical effect of rotating the array of elements in synchronization about parallel axes 24 is equivalent to rotating a larger mirror through the same angle. An advantage of the reticulated mirror rotational scheme is that the extreme ends of the mirror array remain in approximately the same plane as the center elements. Unlike the conventional macroscopic galvanometer mirror, which introduces changes in the optical path length as a result of its rotation about an axis perpendicular to the optical path, the DMD mirror array accomplishes beam steering without changing the optical path length by more than a few microns. While galvanometers result in focus changes and other optical artifacts, the reticulated mirror method eliminates them. Fresnell lenses are constructed on the same principle.

As a result of the ability to individually tilt the long elements of the mirror array under precise electrical control, the array can be used to accomplish the same effect as a reflective Fresnell lens of a cylindrical type (e.g. having optical power along one axis only, and no optical power along the orthogonal axis). Signal generators 37 and 39 (shown in FIGURE 3) may apply a prescribed series of voltage steps to the address electrodes of the parallel rows of mirrors corresponding to an equation describing the desired one dimensional optical surface. For instance, a plane mirror may be modeled by applying generally equivalent voltage levels to each electrode. Other optical surfaces may be modeled by tilting the mirrors a varying amount. This would provide an active, electronically programmable reflective, cylindrical optical element.

It is also possible under control of signal generators 37 and 39 to combine both the effect of the lens and the steering mirror. Light impinging on the surface could then be focused and redirected at the same time. This is possible due to the very high response speed of the DMD monolithic semiconductor type mirror elements.

Although the present invention has been described in detail, it should be understood that various changes, substitutions and alterations can be made hereto without departing from the spirit and scope of the invention as defined by the appended claims.

Claims

1. An apparatus (10) for directing light comprising: a light source (15); a modulator comprising a plurality of individual mirrors (16); and electronic circuitry (37) for generating a signal characteristic of an angle through which each mirror (16) is to be rotated and applying the signal to the mirror (16) by way of at least one address electrode (36, 34) such that when said signal activates said electrode (34, 36) said mirror (16) being attracted to said electrode (36, 34) by electrostatic force, wherein:

each said mirror (16) being rotatably fixed by flexible hinges (30) to at least two support members (22) underneath said mirror, wherein

said support members (22) are displaced from any edge of said mirror, the support members forming an axis of rotation (24).

2. The apparatus of claim 1, wherein the light source (15) further comprises a collimator for producing a light beam before said light impinges upon said modulator.
3. The apparatus of claim 1 or claim 2, wherein the light source is a laser.
4. The apparatus of any of claims 1 to 3, wherein the plurality of modulators are formed on a single substrate.
5. A method of manufacturing a spatial light modulator array as set out in claim 1, said method including the steps of: manufacturing addressing circuitry (37) upon or in a semiconductor substrate (46); depositing, patterning and etching a metal layer to define address electrodes (34, 36) and stops (38) upon said addressing circuitry, wherein said address electrodes respond to signal received by said addressing circuitry; forming support post pads (42) upon said substrate; depositing a spacing material (48) upon said addressing circuitry and said support post pads; etching said spacing material to form vias over said support post pads; depositing a metal layer (52) such that said metal layer fills said vias to form posts, and said metal layer is patterned and etched to form hinges extending from said posts; depositing, patterning and etching a reflective metal layer (56) to form a mirror supported by said hinges; and etching said spacing material such that said mirror is operable to move freely in response to signals received at said addressing circuitry, which activates one of said address electrodes, causing said mirror to rotate upon said support posts;

wherein said support post pads and said support posts are displaced from any edge of said mirror and support said mirror from underneath said mirror by way of said hinges, along a predetermined axis of said rotation.

6. The method of manufacture as claimed in claim 5, wherein said reflective metal layer comprises Ti:Si:Al.
7. The method of manufacture as claimed in claim 5, wherein said step of depositing a metal layer such that said metal layer fills said vias to form posts and wherein said metal layer is patterned and etched to form hinges includes forming end support posts and end hinges (20), such that said end posts and hinges support said mirror from opposite edges of said mirror.

8. The method of manufacture as claimed in claim 5,
wherein said predetermined axis of rotation (24) is
determined to be along the center of said mirror.
9. The method of manufacture as claimed in claim 5, 5
wherein said predetermined axis of rotation (24) is
determined to be along a line offset from the center
of said mirror.
10. The method of manufacture as claimed in claim 5, 10
wherein said method is applied monolithically to an
array of said elements, each element undergoing
the same steps of manufacture at each time,
wherein said address electrodes of each element
are capable of receiving addressing signals unique 15
to that said element.

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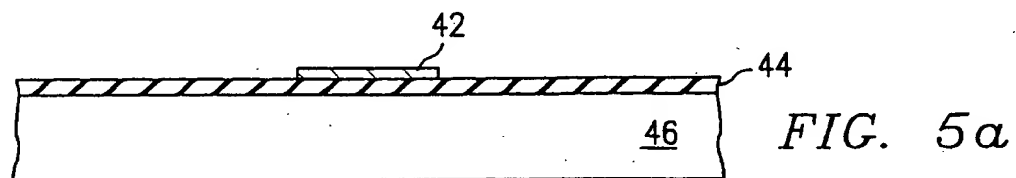
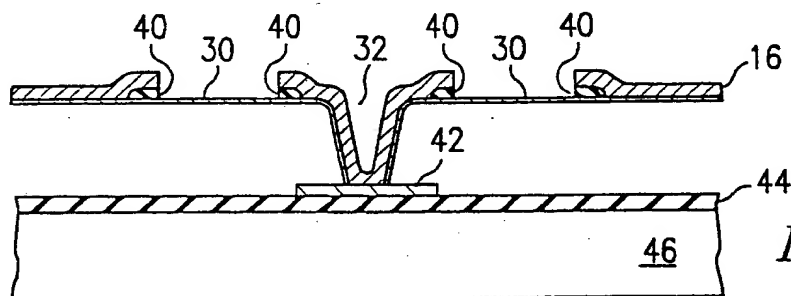
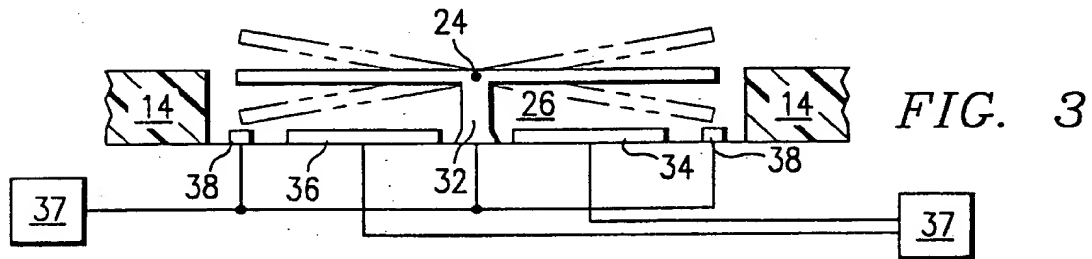
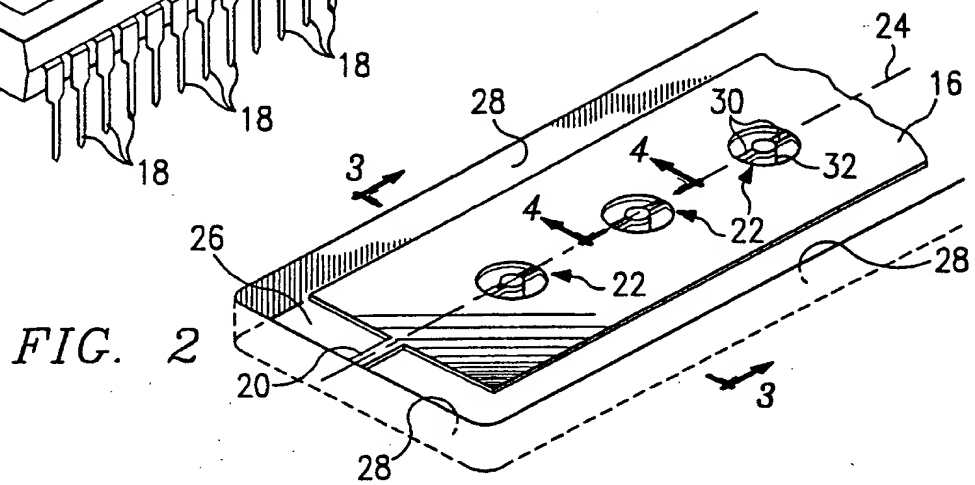
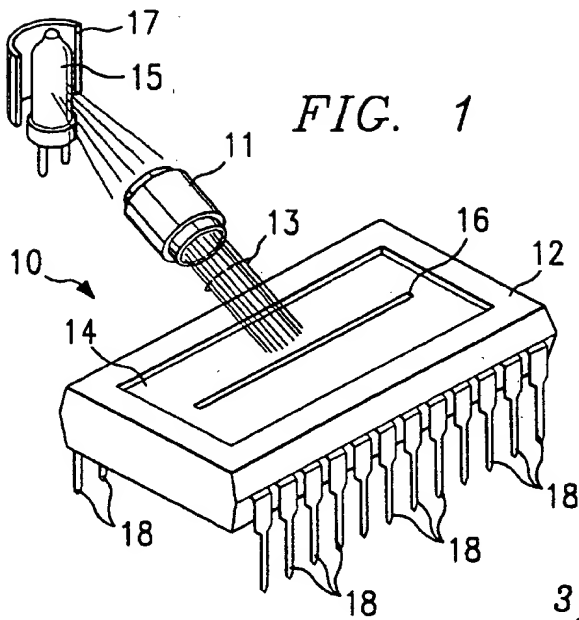
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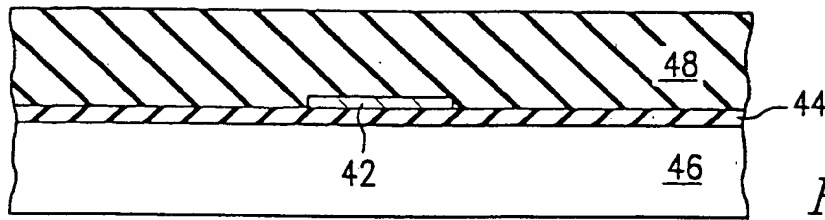


FIG. 5b

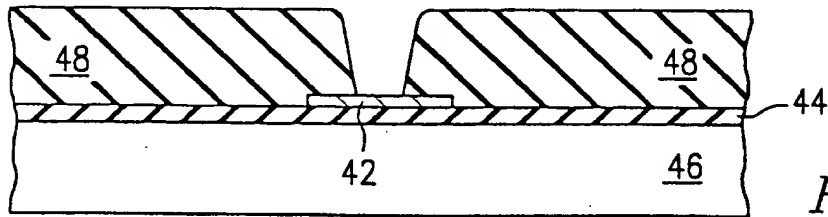


FIG. 5c

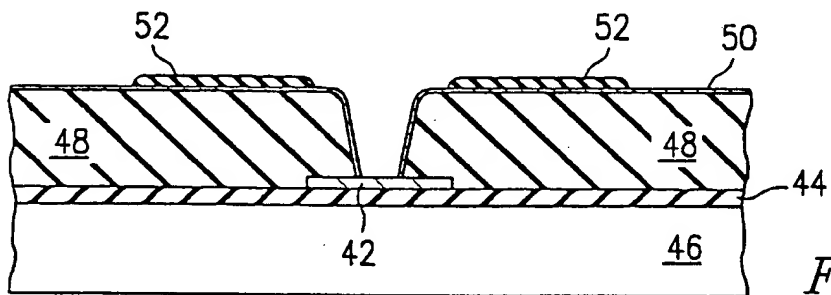


FIG. 5d

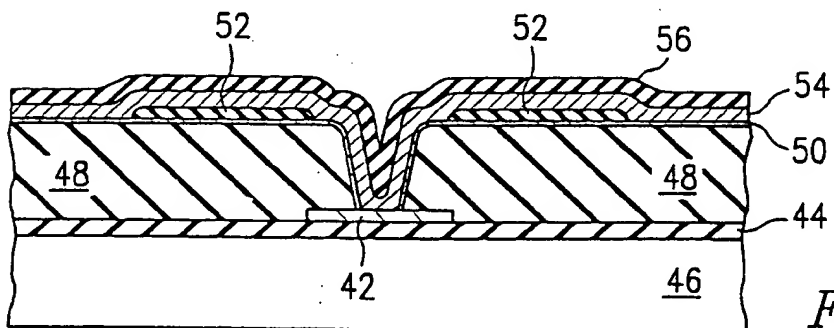


FIG. 5e

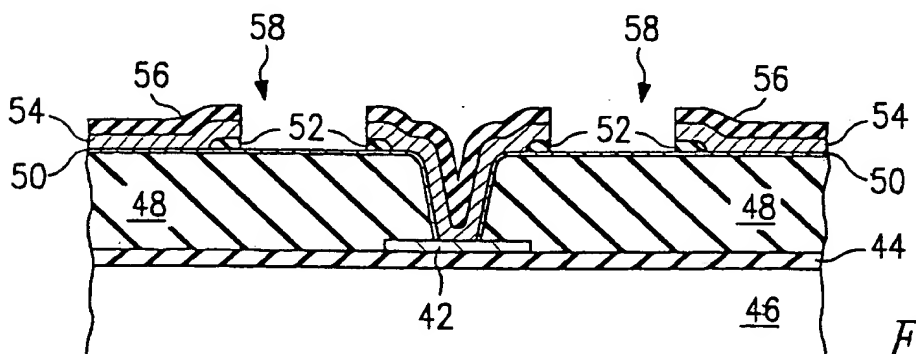
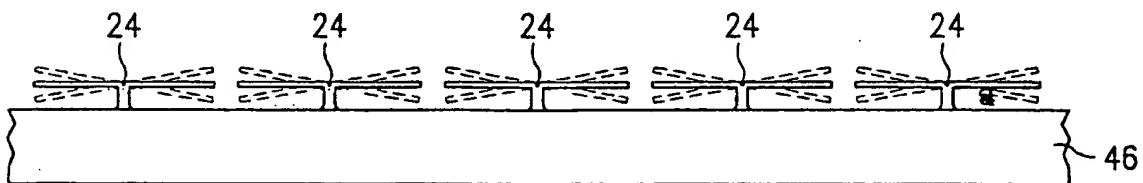
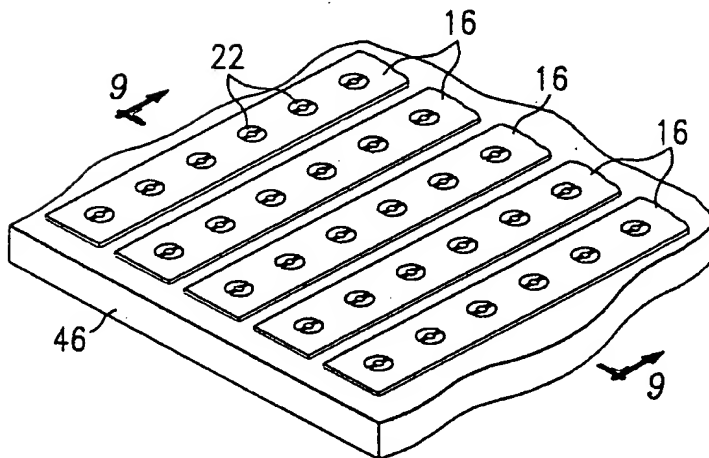
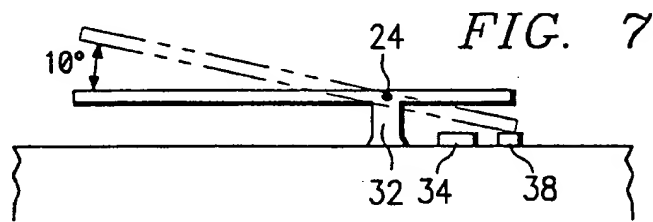
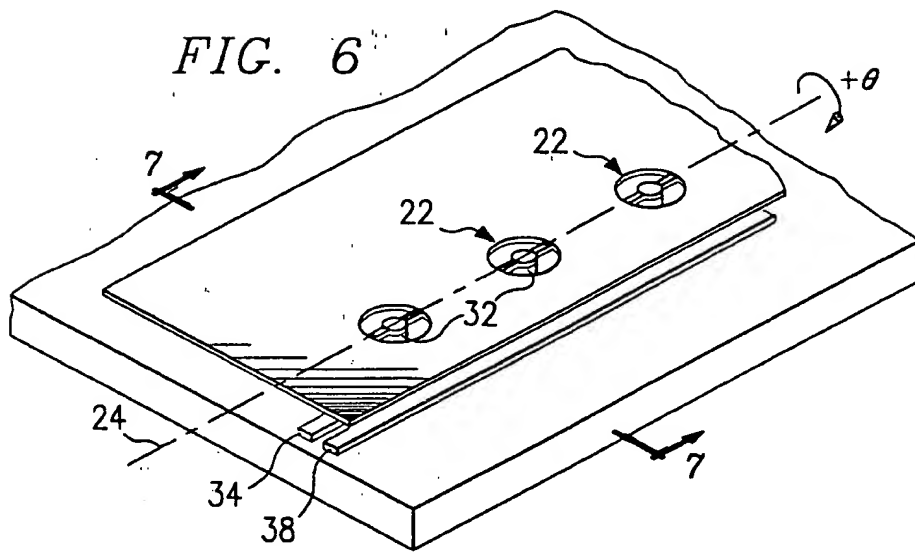


FIG. 5f





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 96 11 0380

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
A	EP-A-0 040 302 (IBM) 25 November 1981 * page 4 - page 5; figures 2,3,7 * ---	1,4,5,7, 8,10	G02B26/08 G09F9/37
A	SPATIAL LIGHT MODULATORS AND APPLICATIONS III, 7-8 AUGUST 1989, SAN DIEGO, vol. 1150, 7 August 1989, pages 86-102, XP000351394 HORNBECK L J: "DEFORMABLE-MIRROR SPATIAL LIGHT MODULATORS" * page 88 - page 89; figures 2,4,6,29 * ---	1-6	
A	JOURNAL OF PHYSICS E. SCIENTIFIC INSTRUMENTS, vol. 21, no. 7, July 1988, pages 680-685, XP000005638 GUSTAFSSON K ET AL: "A SILICON LIGHT MODULATOR" * figures 1,3 * ---	1,3-5,7, 10	
P,A	US-A-5 085 497 (UM GREGORY ET AL) 4 February 1992 * column 7, line 37 - column 9, line 2; figures 11-13 * -----	1,4,5,10	TECHNICAL FIELDS SEARCHED (Int.Cl.6) G02B G09F
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 7 August 1996	Examiner von Moers, F
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

EPO FORM 1503 01.82 (P04001)